

# TECHNICAL DATA, FORMULAS AND CHARTS

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Diagram for local district heating plants connected to a heating and power plant.

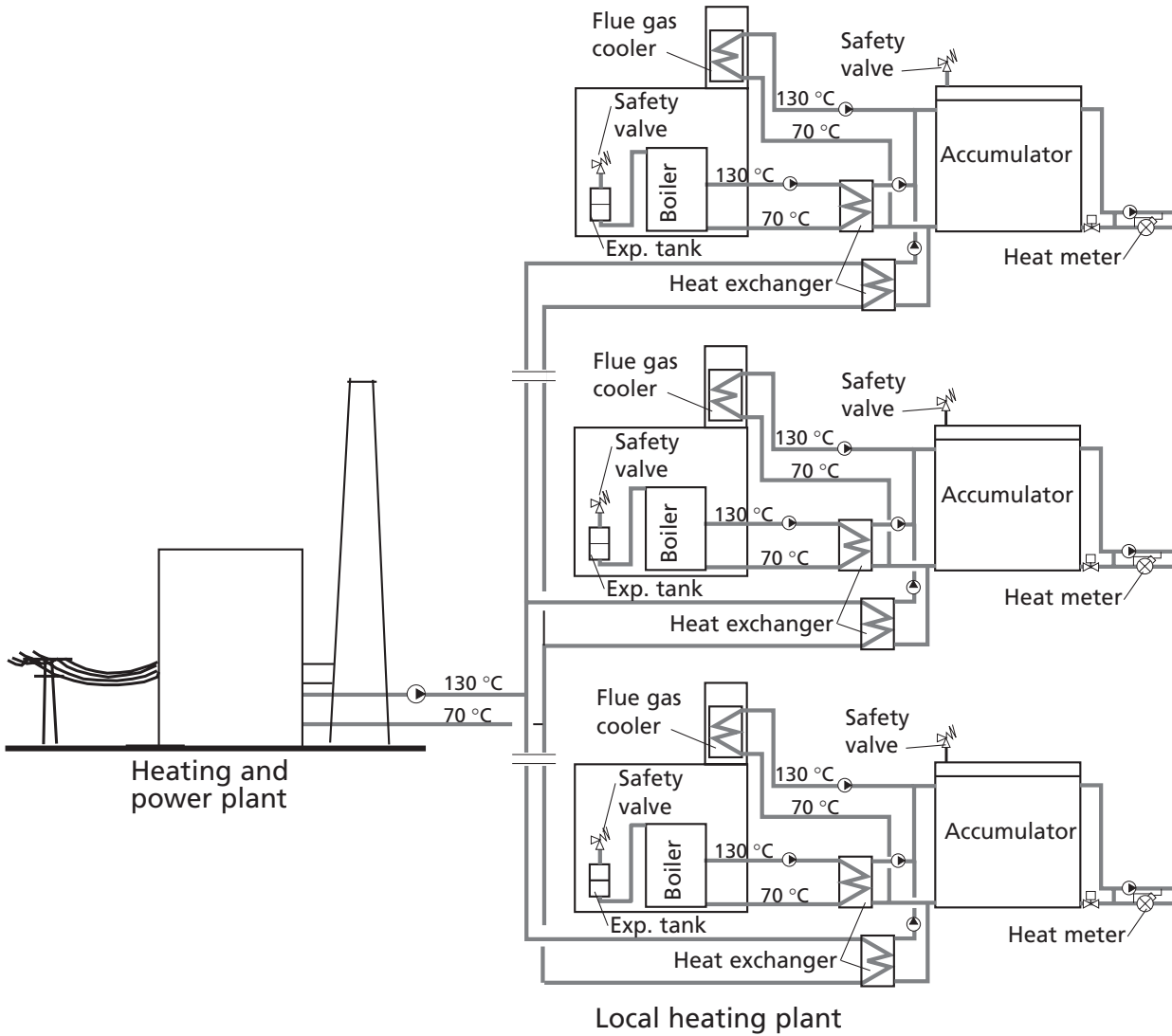
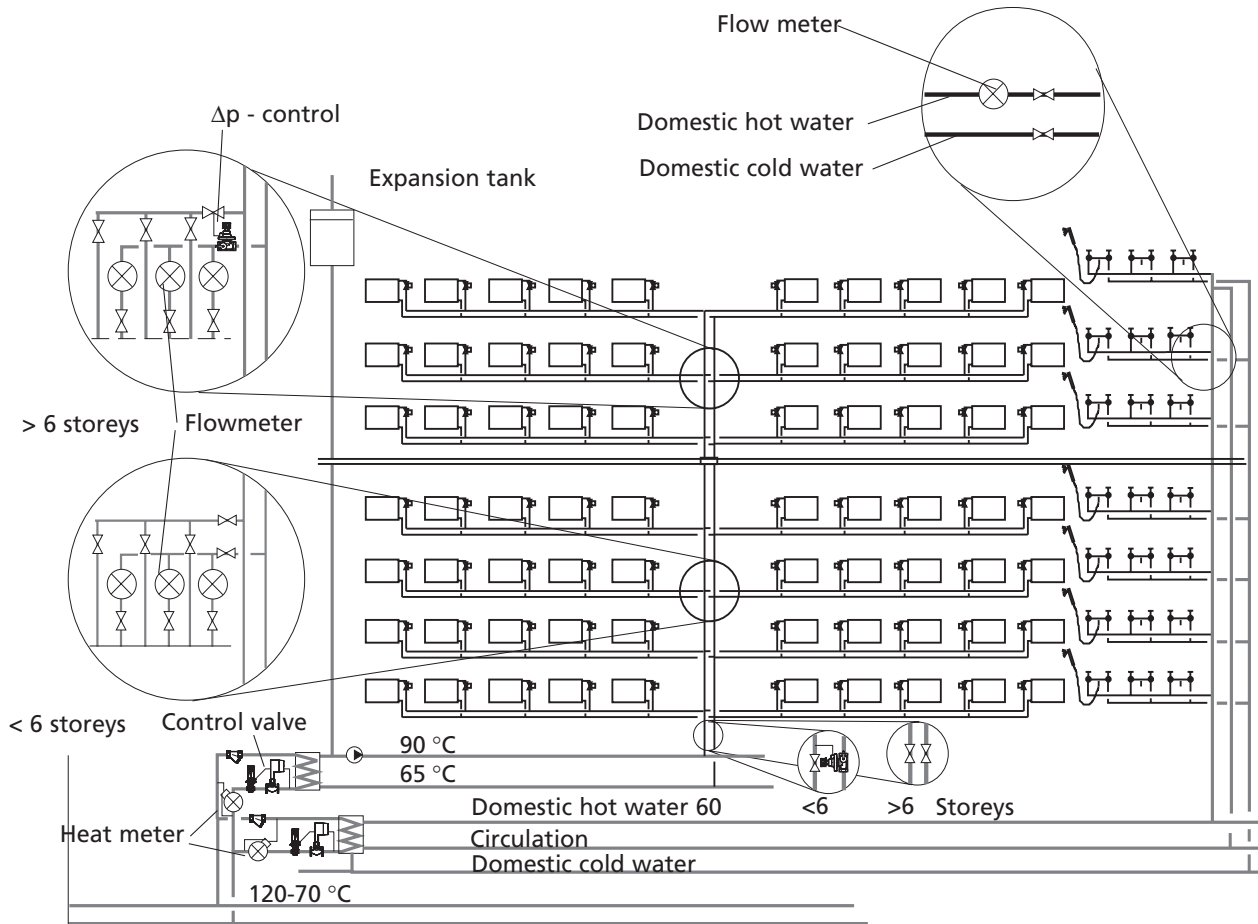


Diagram for heating and domestic hot and cold water.



Heat emission from radiators.

Two-pipe system with thermostatic valves.

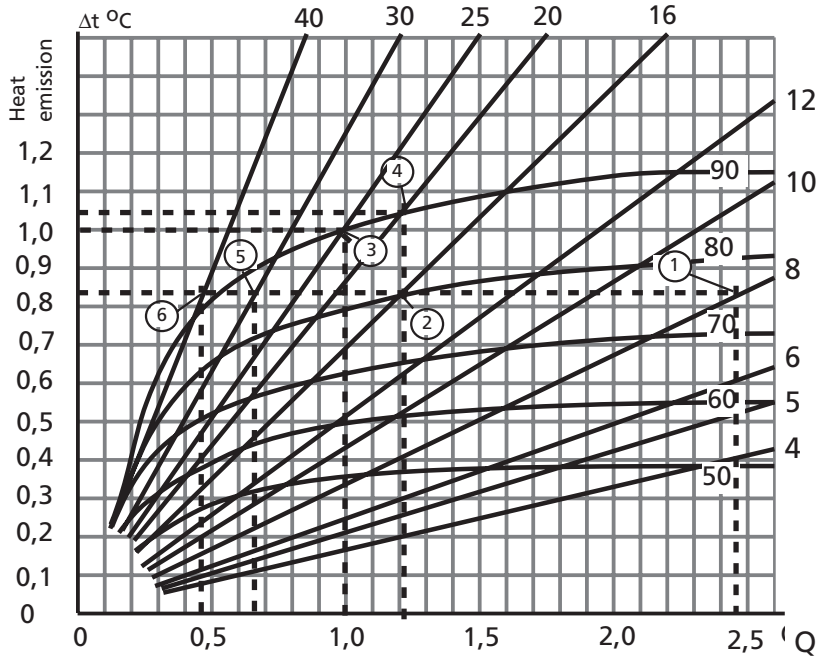
Measured ① :  $t_{flow} 75^{\circ}C$ ,  $\Delta t 8^{\circ}C$

Heat requirement : 0,83,  $Q = 2,47$

$t_{flow} 80^{\circ}C$  : ②  $\Delta t 16^{\circ}C$ ,  $Q = 1,23$

Every point along the horizontal line 0,83 gives the same heat emission.

$$n = 1,3 \quad t_{room} = 20^{\circ}C \quad t_{flow} = 90^{\circ}C \quad \Delta t = 25^{\circ}C$$



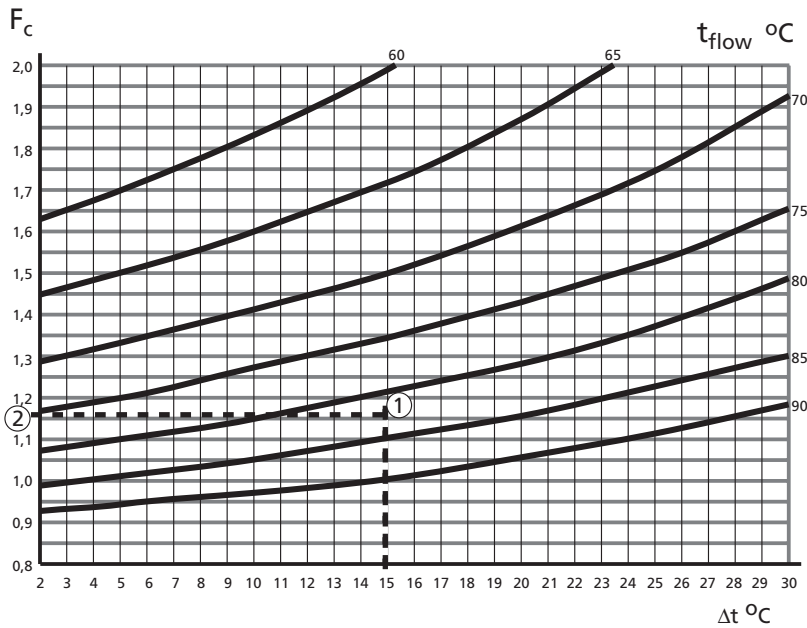
The influence of gravity forces on heat emission from a radiator in a two-pipe system

For a correctly sized radiator ③ ( with manual radiator valve in a two-pipe system ) the heat emission will increase only by 5% when the flow increases by 23%, ④, depending on gravity forces. The temperature drop across the radiator however will decrease by 5°C and that is significant, because it reduces the capacity of the whole system all the way down to the heating and power plant.

Results  $\Delta t$  for one- and two - pipe circuits, and required pump capacity when thermostatic valves utilize internal and external heat gains.

Point	Two-pipe circuit					One-pipe circuit		
	Heat gain %	Flow %	$\Delta t$ °C	Circuit resistance %	Pump capacity %	Flow %	$\Delta t$ °C	Pump capacity %
③	0	100	25	100	100	100	25	100
⑤	10	66	33	44	29	100	22,5	100
⑥	20	47	39	22	10	100	20	100

Conversion chart for radiators in one-pipe circuits.



Conversion chart for panel and section radiators in one-pipe circuits. Enter the current  $t_{flow}$  and temperature drop and find the conversion factor,  $F_c$ .

Multiply the heat requirement by  $F_c$  and select size of the radiator according to the new value.

Example.

Calculated heat requirement: 1.230 W.

$t_{flow}$  : 82 °C,  $\Delta t$ : 15 °C, ①

$F_c = 1,16$  ②

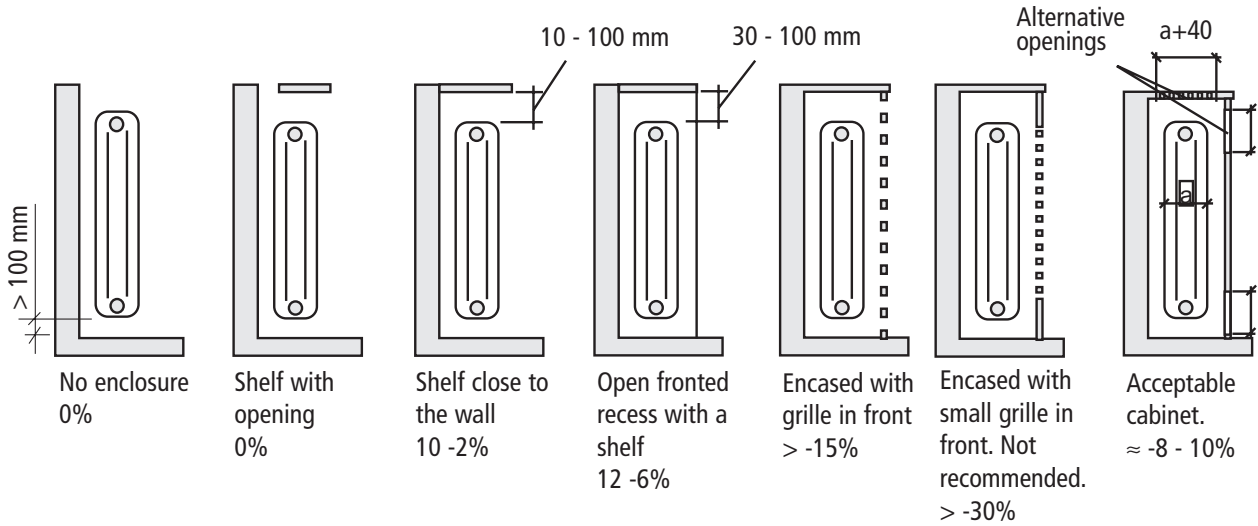
Converted heat requirement:  $1.230 \times 1,16 = 1.427$  W.

Formula for calculating  $F_c$ :

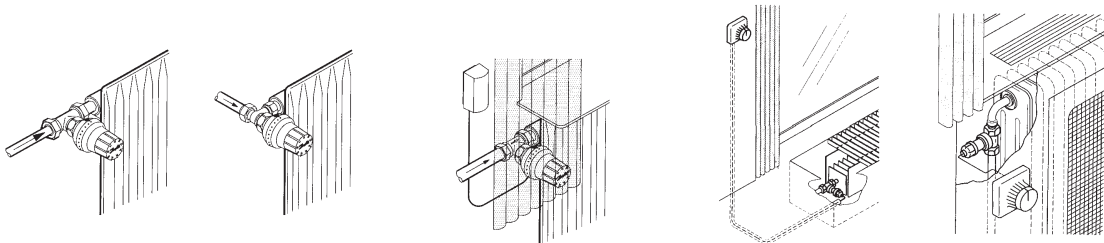
$$F = \left[ \frac{49,33 \times \ln \left( \frac{t_1 - t_r}{t_2 - t_r} \right)}{t_1 - t_2} \right]^n$$

Panel radiator	n
Section radiator	1,28
Convactor	1,29
	1,3 - 1,33

Reduction of heat emission from radiators fixed in some type of enclosure



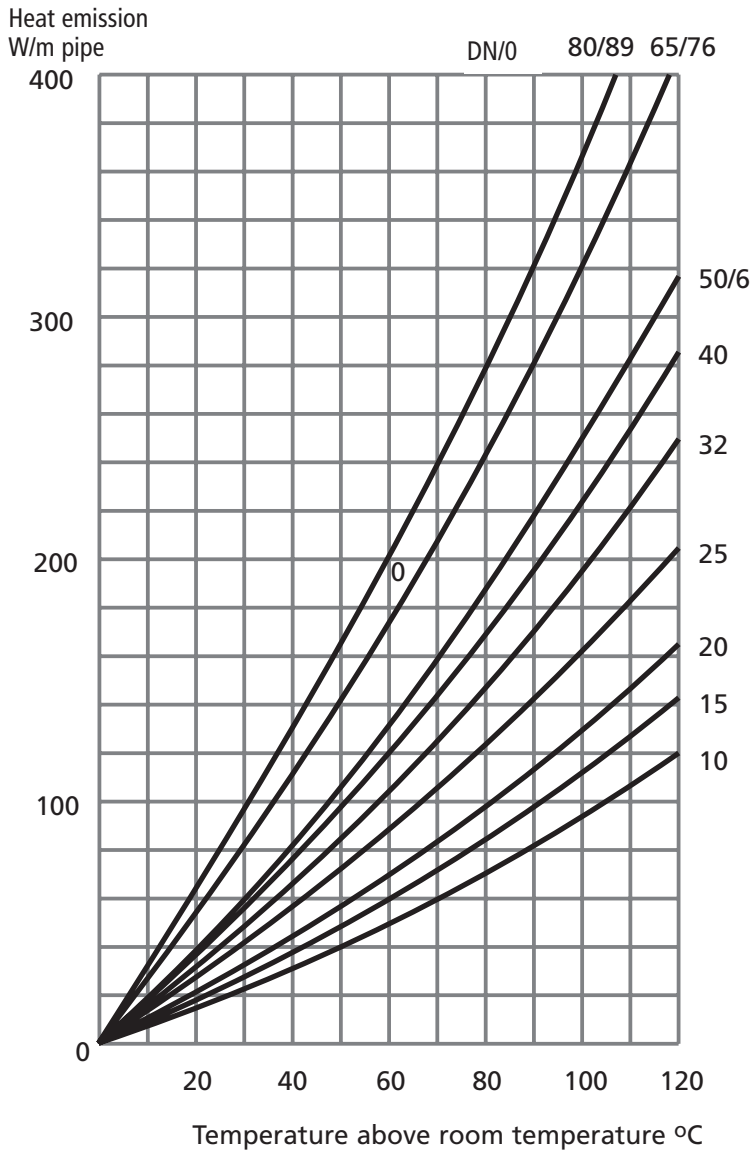
The control unit has to sense the room temperature to be able to control it.



Radiation from a radiator depending on the treatment of the surface.

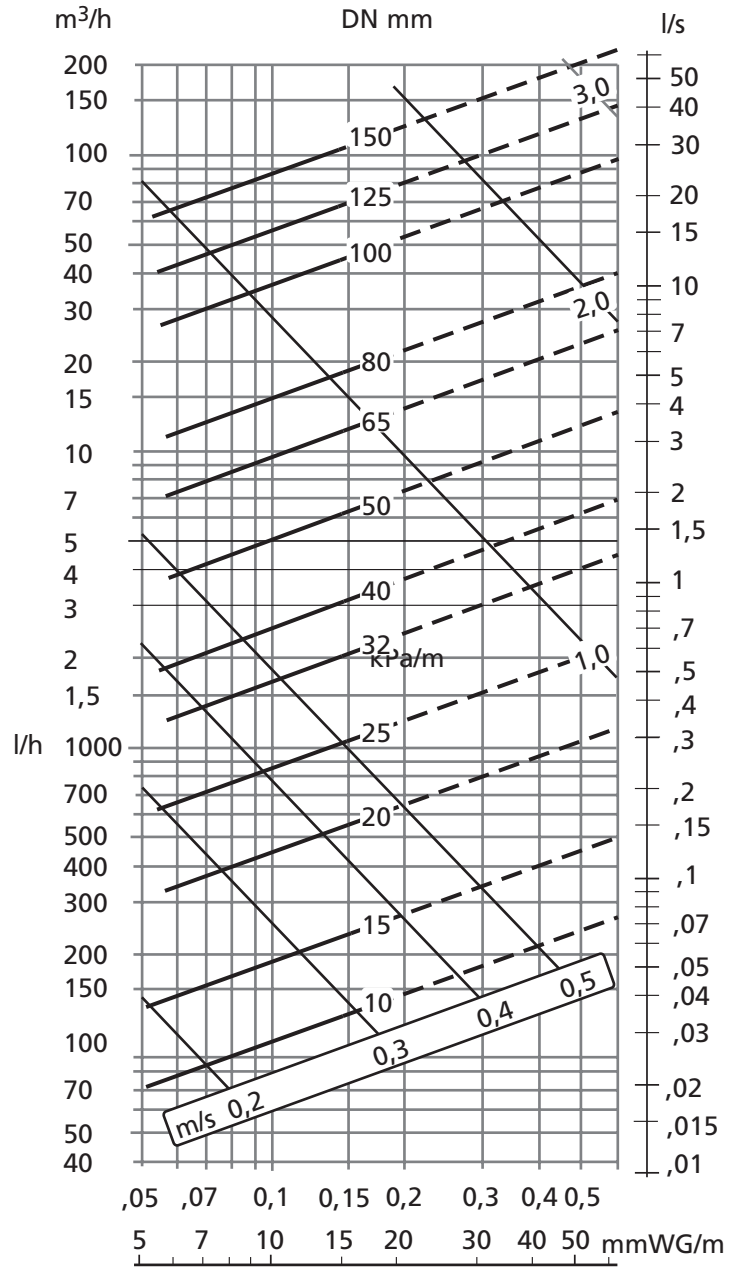
Material	Surface treatment	Radiation %
Steel, cast iron		100
	Oil paint	100
	Aluminium or copper bronzes	75
	Zinc white	101
	Lead white	99
Enamelled	White	101
	Matt green	96
Aluminium		8

Heat losses from uninsulated horizontal pipe.



For vertical pipe reduce by 20%  
 One-pipe above another reduce by 12%  
 Three pipes above each other reduce by 20%

Pressure drop in steel pipes for heating installations.



$k = 0,00003 \text{ m}$   
 Density =  $1.000 \text{ kg/m}^3$

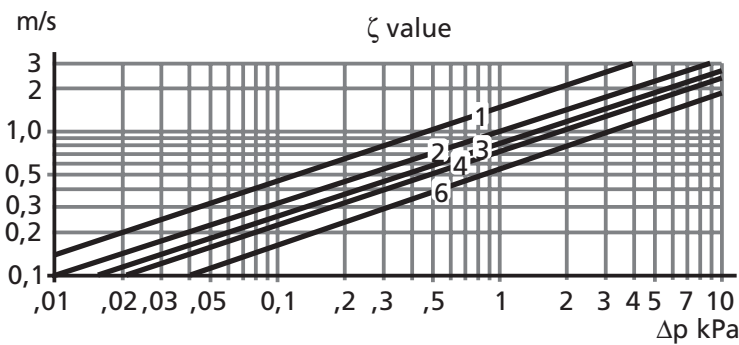


$\Delta p$  for  $\zeta$  values at different rates.

Symbol	Units	Coefficient of resistance, $\zeta$
	Branch tee	1
	Through tee	1
	Elbow, smooth	0,2
	Bend	1

The values for the coefficient of resistance for tees, elbows and bends.

The pressure drop is calculated from:  
 $\Delta p = \zeta 0,5 \rho v^2$ ,



Recommended portion of pipe losses for different systems or part of systems.

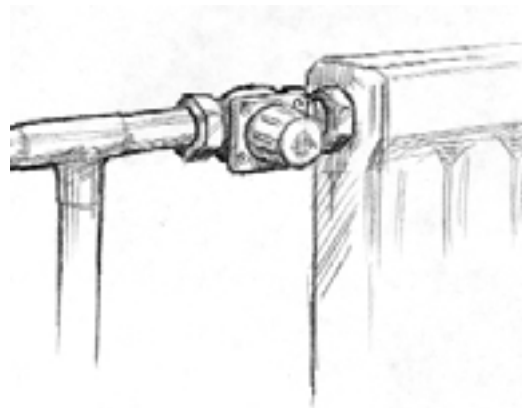
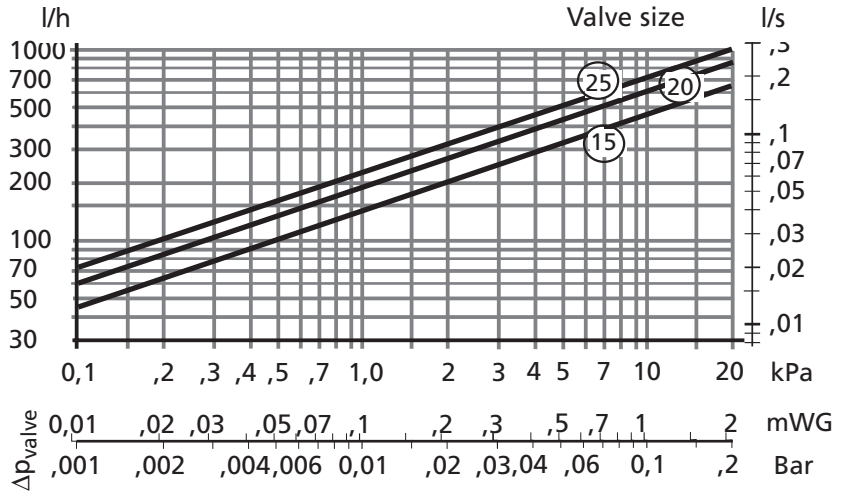
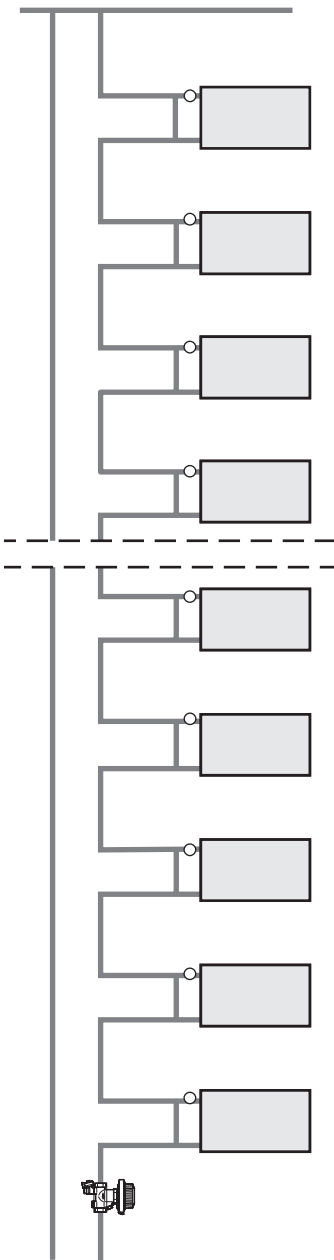
Type of system	Unit	Friction %
Heating	Small buildings	50 - 60
	Large buildings	60 - 70
Sub-stations	Primary and secondary side	20 - 30
Distribution pipe net work	Primary side	80 - 90

Sizes of steel pipes for heating systems. Working pressure 1,0 MPa (10 bar)

Nominal diameter	External diameter	Wall thickness	Internal diameter
mm	inch	mm	mm
8	1/4	13,50	2,25
10	3/8	17,00	2,25
15	1/2	21,25	2,75
20	3/4	26,75	2,75
25	1	33,50	3,25
32	1 1/4	42,25	3,25
40	1 1/2	48,00	3,50
50	2	60,00	3,50
65	2 1/2	75,50	3,75
80	3	88,50	4,00
100	4	114,00	4,00
125	5	140,00	4,50
150	6	165,00	4,50

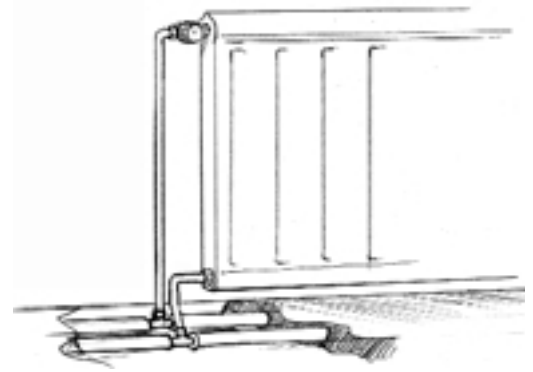
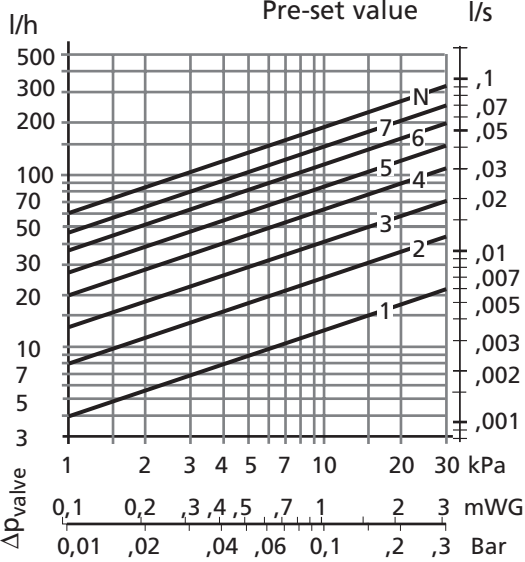
Flow chart for RTD-G 15, 20 and 25

RTD - G 15, 20 and 25



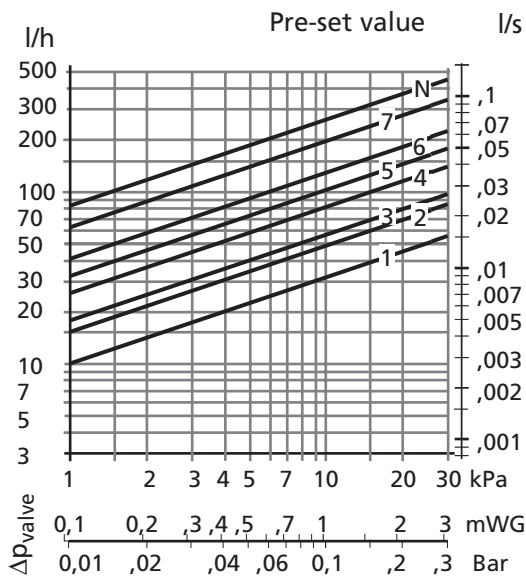
Flow chart for thermostatic valves in two-pipe system

RTD - N 15



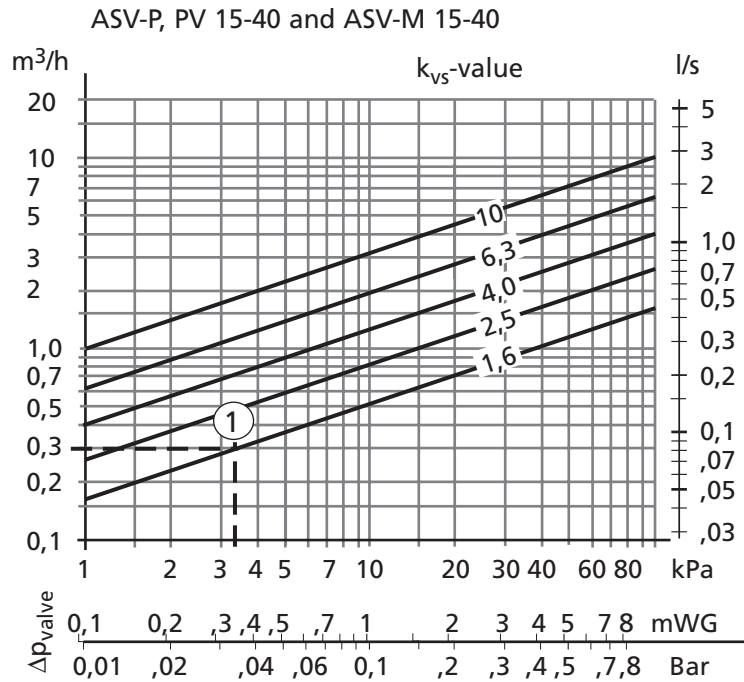
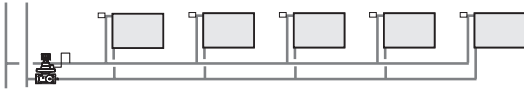
Pre-set value	1	2	3	4	5	6	7	N
kv values	0,04	0,08	0,12	0,20	0,27	0,36	0,45	0,60

RTD - N 20 - 25



Pre-set value	1	2	3	4	5	6	7	N
kv values	0,10	0,15	0,17	0,25	0,32	0,41	0,62	0,83

Flow chart for  $\Delta p$  control valves for riser or circuit in heating systems.



Working range:

ASV-P 10 kPa

ASV-PV 5 - 25 kPa.

Minimum available  $\Delta p$  for good functioning: 8 kPa.

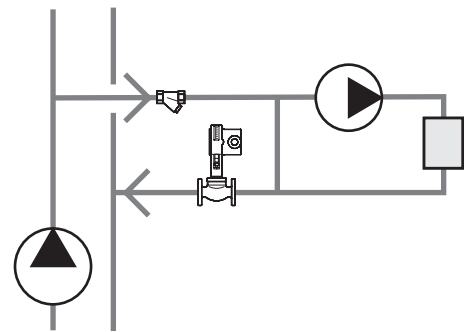
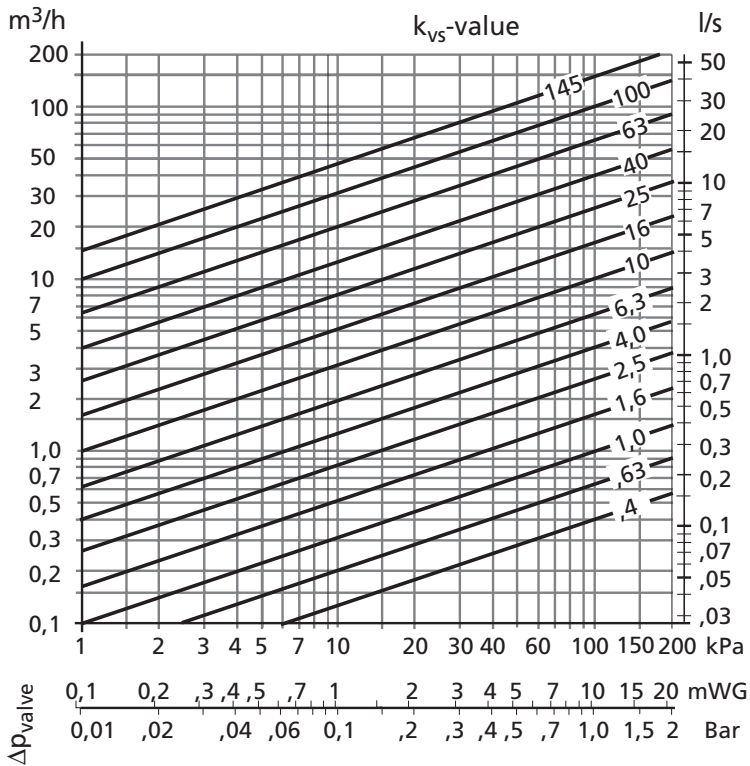
Example

Q: 300 l/h.  $\Delta p$  riser: 7kPa.  $\Delta p$  radiator including valve: 5 kPa.

$\Delta p$ -control kv 1,6.  $\Delta p_{vp} = 3,4$  kPa, ①

Necessary  $\Delta p = 7+5+8 = 20$  kPa.

Flow chart for control valves in heating systems.



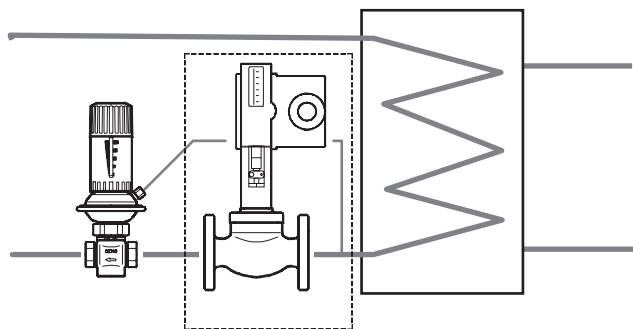
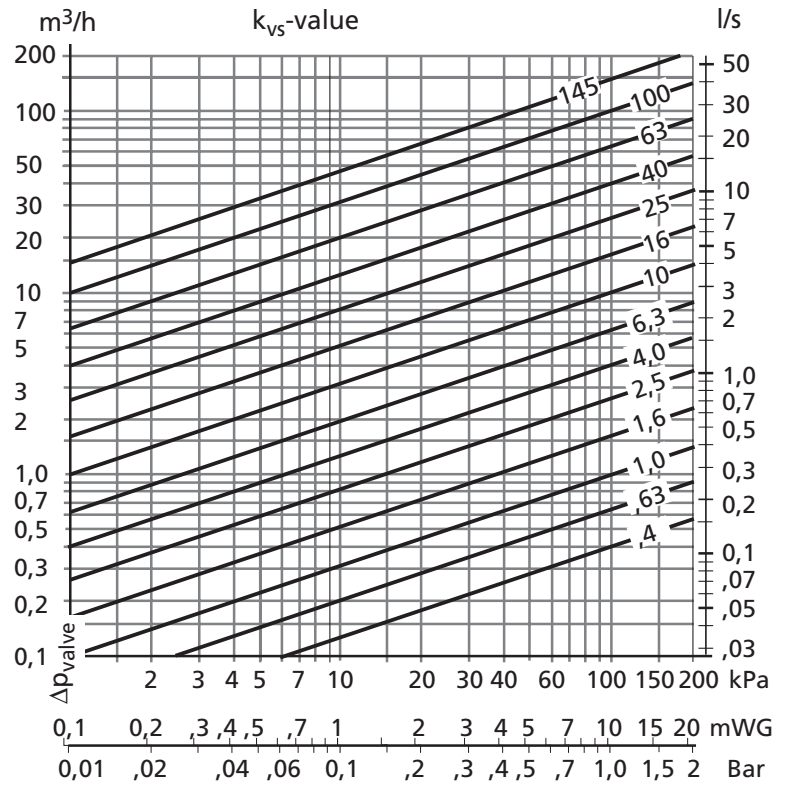
Formulas.

$$\Delta p : \text{bar. } Q: \text{ m}^3/\text{h. } k_v = \frac{Q}{\sqrt{\Delta p}} ; \Delta p = \left(\frac{Q}{k_v}\right)^2 ; Q = k_v \sqrt{\Delta p} ;$$

$$\Delta p : \text{kPa. } Q: \text{ l/h. } k_v = 0,01 \frac{Q}{\sqrt{\Delta p}} ; \Delta p = \left(0,01 \frac{Q}{k_v}\right)^2 ; Q = 100 \times k_v \sqrt{\Delta p} ;$$

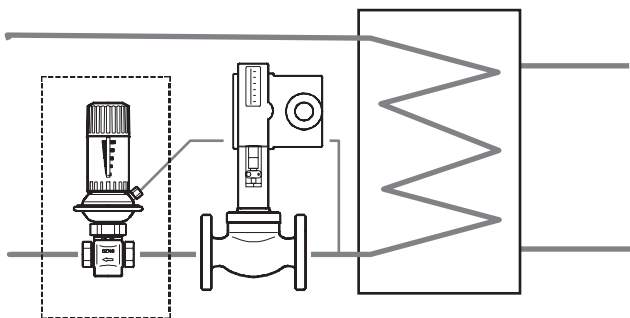
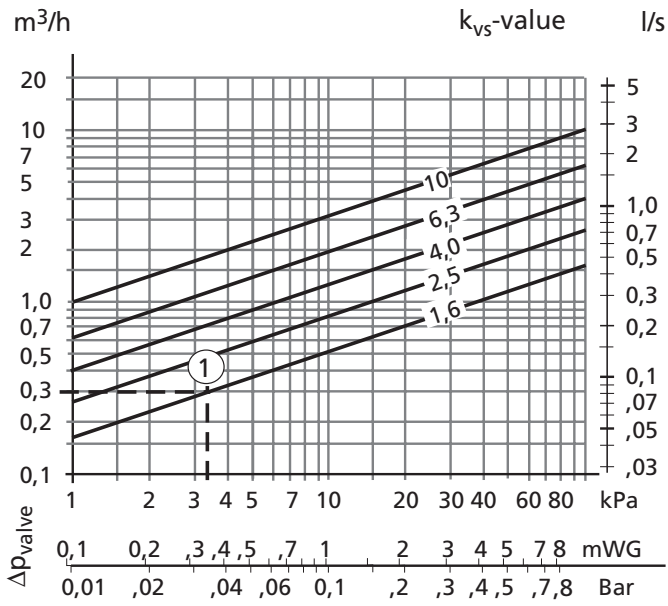
$$\Delta p : \text{kPa. } Q: \text{ l/s. } k_v = 36 \frac{Q}{\sqrt{\Delta p}} ; \Delta p = \left(36 \frac{Q}{k_v}\right)^2 ; Q = \frac{k_v}{36} \sqrt{\Delta p} ;$$

Flow chart for valves in district heating systems.



Flow chart for  $\Delta p$  control valves in district heating systems.

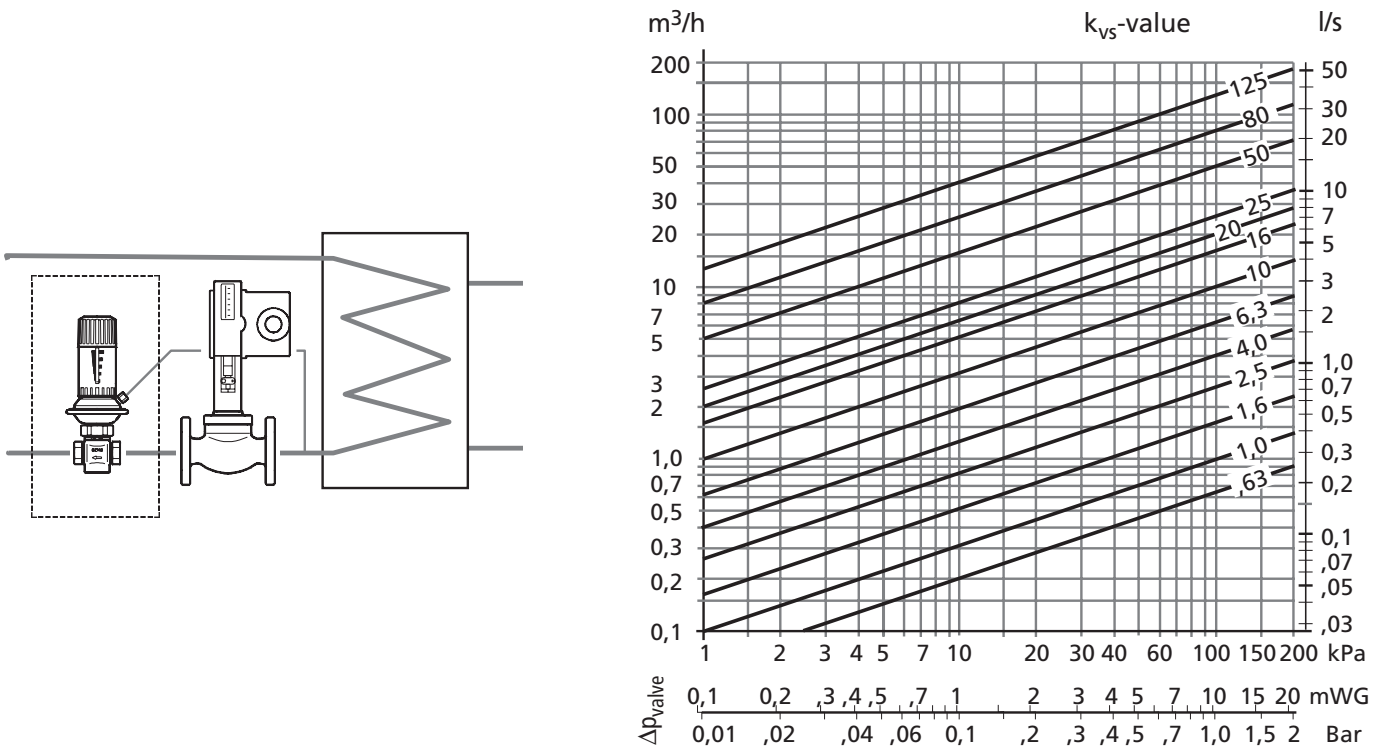
AVP 15 - 32



Flow chart for  $\Delta p$  control valves in district heating systems.

IVD-IVFS  $k_{VS}$  0,63 - 25,0  $m^3/h$

AFP  $k_{VS}$  50 - 125  $m^3/h$



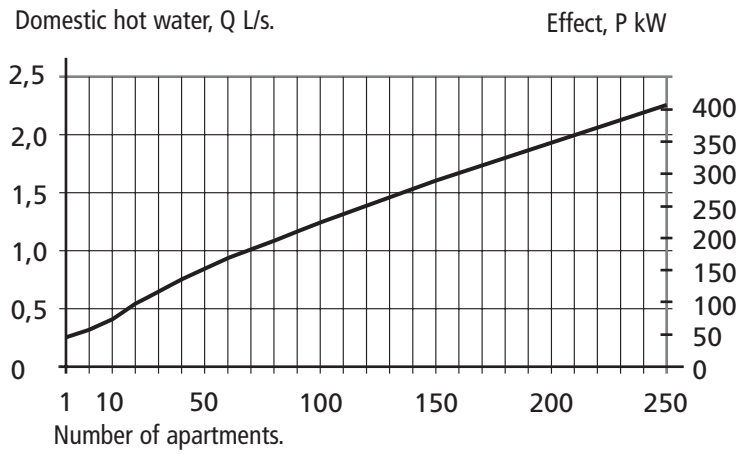
$\Delta p$ -regulator, working range: IVD 5 - 50 and 20 - 250 kPa.  
AFP 20 - 120 and 50 - 250 kPa

Maximum  $\Delta p$  valve IVF  $k_{VS}$ : 0,63 and 1,0 = 1.000 kPa  
2,5 = 630 kPa  
4,0 - 25 = 800 kPa

Maximum  $\Delta p$  valve AFP: 1.200 kPa

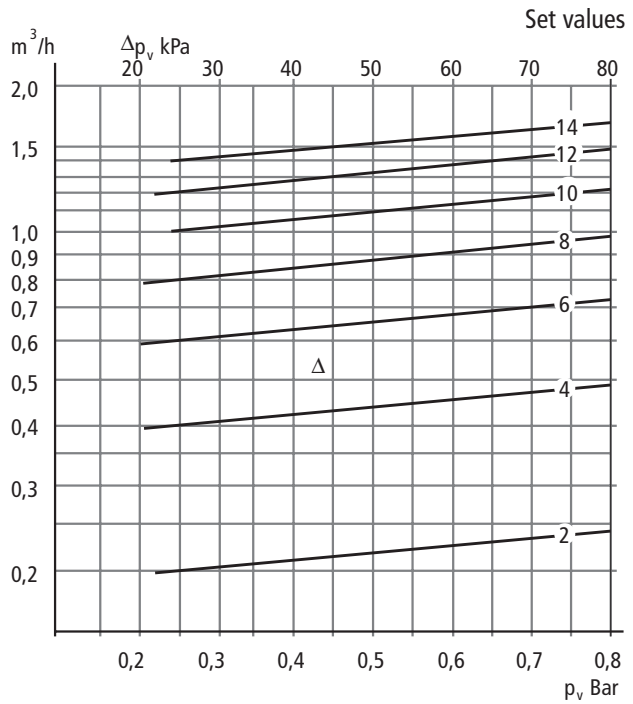
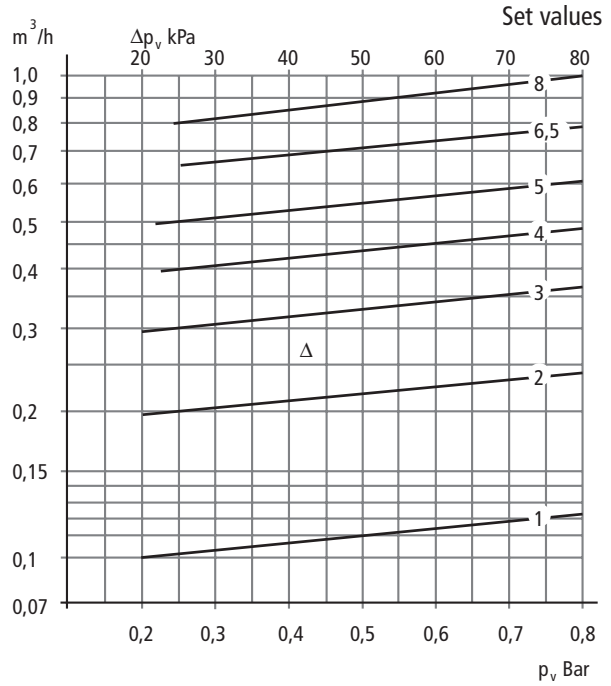


## Heat requirement for hot water according to the Swedish Board of District Heating

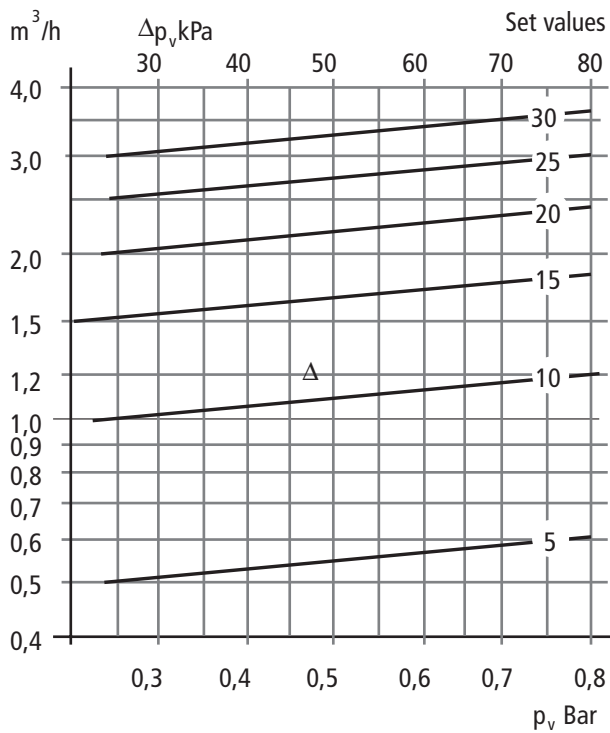
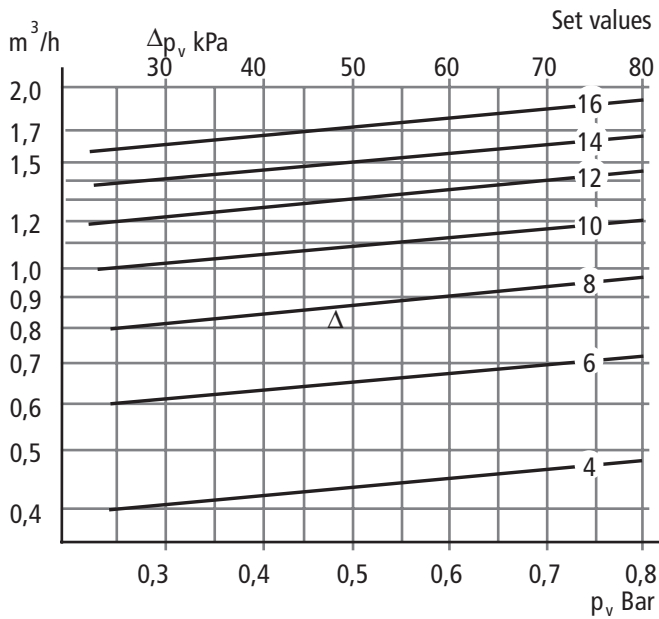


Flow limiter, ASV-Q 15, Flow limiter, ASV-Q 20

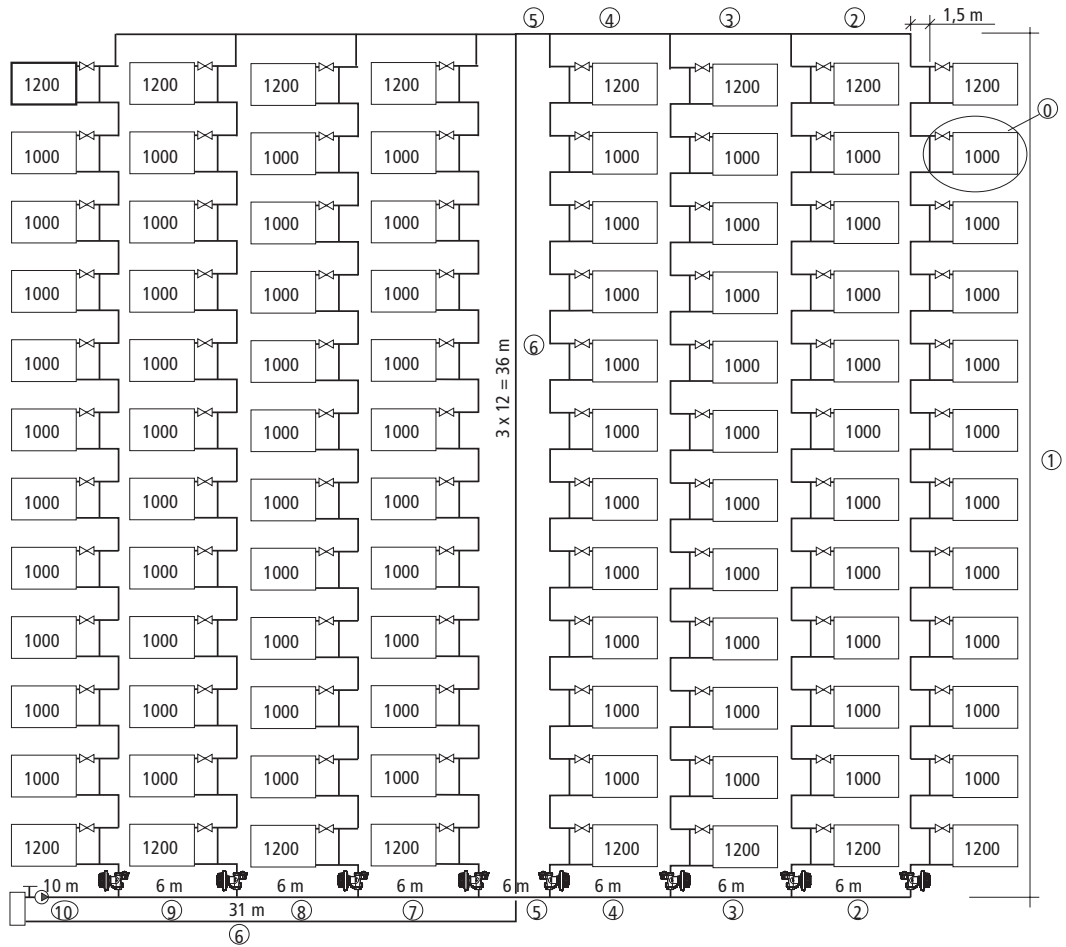
ASV-Q	Capacity l/h	Set value
15	100 - 800	1 - 8
20	200 - 1400	2 - 14
25	400 - 1600	4 - 16
32	500 - 2500	5 - 30



Flow limiter, ASV-Q 25, Flow limiter, ASV-Q 32



Calculation of one-pipe system



Calculation of one-pipe system

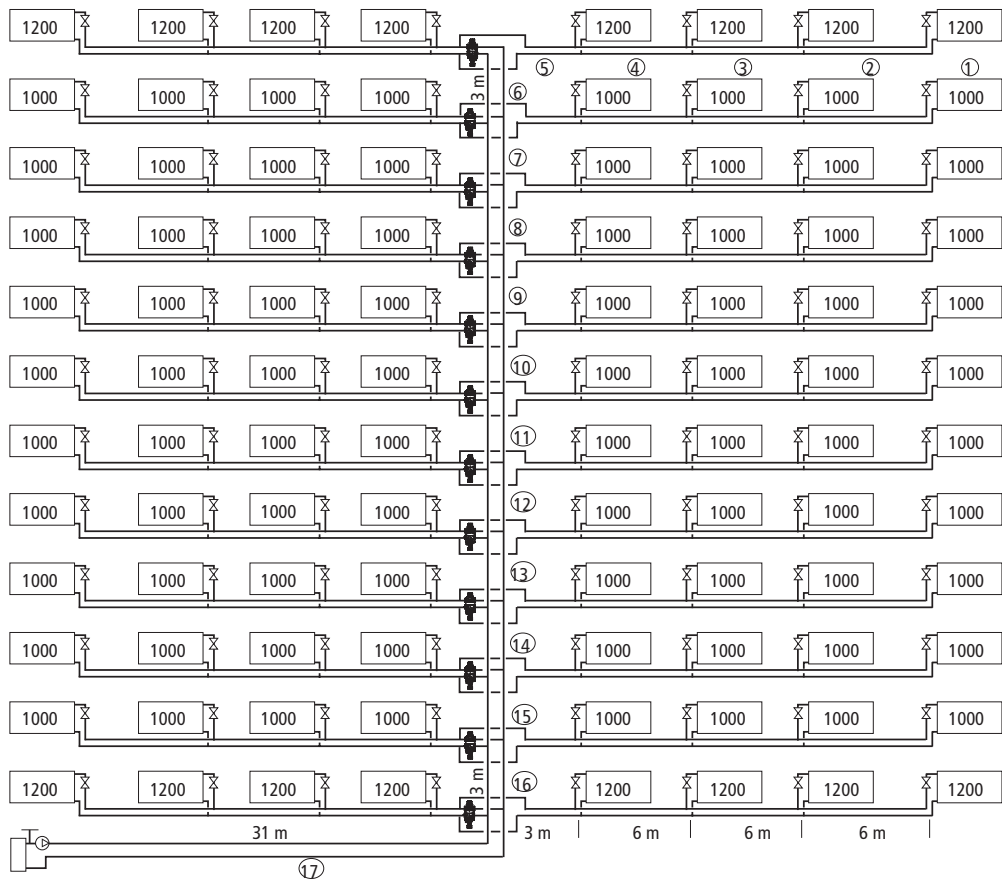
Pos. no	Heat load W	Flow l/h $\Delta t$ 25 °C	Pipe length l m	Pipe size	Velocity m/s	R/m kPa	$\Sigma \zeta$	R x l kPa	Z	R x l + Z kPa	Accum kPa	
0	Resistance across 1 radiator (kv=2) at 30 % flow (427x0,3=128 l/h)			$\Delta p_{rad} = (0,128/2)^2$ ; $\Delta p = 0,0041$ bar=0,41 kPa			Valve 20. $\Delta p_{valve} = 0,48$ kPa		$\Sigma \zeta = 4$ ; Gives 0,2 kPa		1,1x12 = 13,2	
1	12400	427	12x3+12x3=72	20	0,33	0,1		7,2	13,2	20,4	20,4	
ASV-Q	12400	427		20						45	65,4*	
2	12400	427	12	20	0,33	0,1	2	1,2	0,1	1,3	66,7	
3	24800	854	12	25	0,41	0,1	2	1,2	0,1	1,3	68,0	
4	37200	1281	12	32	0,37	0,06	2	0,7	0,2	0,9	68,9	
5	49600	1708	9	32	0,52	0,11	2	1	0,3	1,3	70,2	
6	99200	3413	67	50	0,44	0,05	2	3,4	0,2	3,6	73,8	
7	62000	2133	6	40	0,48	0,06	1	0,4	0,12	0,5	74,3	
8	74400	2559	6	40	0,55	0,12	1	0,7	0,13	0,8	75,1	
9	86800	2986	6	40	0,7	0,14	1	0,8	0,2	1,0	76,1	
10	99200	3413	10	50	0,44	0,05	1	0,5	0,1	0,6	76,7	
Heat exchanger										15	91,7	
Pump: Q= 3.413 l/h, pump head=92 kPa.												
15 % through the radiators give:												
0	Resistance across 1 radiator (kv=2) at 15 % flow (427x0,15=64 l/h)			$\Delta p_{rad} = (0,064/2)^2$ ; $\Delta p = 0,001$ bar=0,1 kPa			Valve 20. $\Delta p_{valve} = 0,2$ kPa		$\Sigma \zeta = 4$ ; Gives 0,01 kPa		0,3x12 = 3,6	

\* The flow limiting valve ASV-Q keeps the flow constant, independent of varying available pressure.

Required pump capacity for the calculated system two- and one-pipe types respectively when thermostatic valves utilizes internal and external heat gains.

Heat gain %	Two-pipe circuit				One-pipe circuit		
	Flow %	$\Delta t$ °C	Circuit resistance %	Pump capacity %	Flow %	$\Delta t$ °C	Pump capacity %
0	100	25	100	100	100	25	100
10	66	33	44	29	100	22,5	100
20	47	39	22	10	100	20	100

Calculation of two-pipe system



Calculation of two-pipe system

Pos. no	Heat load W	Flow l/h $\Delta t$ 25° C	Pipe length l m	Pipe size	Velocity m/s	R/m kPa	$\Sigma \zeta$	R x l kPa	Z kPa	R x l + Z kPa	Accum. kPa
1	1200	41,3		15						1,2	1,2
2	1200	41,3	12	15	< 0,1	0,01	< 1	0,1	0,01	0,1	1,3
3	2400	82,6	12	15	< 0,1	0,02	2	0,2	0,02	0,2	1,5
4	3600	124	12	15	< 0,2	0,05	2	0,6	0,04	0,6	2,1
5	4800	165	6	15	0,24	0,08	2	0,5	0,06	0,6	2,7
ASV-P	9600	330		15						18	18,0*
6	9600	330	6	20	0,25	0,08	2	0,5	0,06	0,6	18,6
7	17600	605	6	20	0,45	0,17	2	1	0,2	1,2	19,8
8	25600	880	6	25	0,41	0,11	2	0,7	0,15	0,9	20,7
9	33600	1156	6	25	0,5	0,13	2	0,8	0,25	1	21,7
10	41600	1431	6	32	0,4	0,07	2	0,4	0,15	0,7	22,4
11	49600	1706	6	32	0,5	0,1	2	0,6	0,25	0,9	23,3
12	57600	1981	6	40	0,41	0,06	2	0,4	0,15	0,6	23,9
13	65600	2257	6	40	0,5	0,09	2	0,5	0,25	0,8	24,7
14	73600	2532	6	40	0,55	0,11	2	0,7	0,30	1	25,7
15	81600	2807	6	40	0,6	0,13	2	0,8	0,35	1,2	26,9
16	89600	3082	6	40	0,65	0,16	2	1	0,4	1,4	28,3
17	99200	3413	62	50	0,45	0,05	4	3,1	0,4	3,5	31,8
Heat exchanger											
Pump: Q = 3.413 l/h, pump head 47 kPa.											
Resistance in the small circuit with 1000 W per radiator.											
1	1000	34		15							
2	1000	34	12	15	< 0,1	0,01	2	0,1	-	0,1	
3	2000	69	12	15	< 0,1	0,015	2	0,2	-	0,2	
4	3000	103	12	15	0,15	0,03	2	0,4	0,02	0,4	
5	4000	138	6	15	0,2	0,05	2	0,3	0,04	0,3	

\* The differential pressure valve ASV-P keep  $\Delta p$  across the radiator circuits at 10 kPa and need another 8 kPa minimum for good functioning.

Pre-set values for the radiators in the calculated circuit.			Pre-set values for the small circuits with 1000 W per radiator.		
Radiator no	Available $\Delta p$ kPa	Pre-set value	Radiator no	Available $\Delta p$ kPa	Pre-set value
4	10 - 0,6 = 9,4	3	4	10 - 0,3 = 9,7	2,5
3	9,4 - 0,6 = 8,8	3	3	9,7 - 0,4 = 9,3	2,5
2	8,8 - 0,2 = 8,6	3	2	9,3 - 0,2 = 9,1	3,0
1	8,6 - 0,1 = 8,5	3	1	9,1 - 0,1 = 9,0	3,0

Thanks to the differential pressure valve ASV-P all circuits have the same  $\Delta p$  available, 10 kPa.

**SI-units.**
**Effect, P.**

<b>W</b>	<b>kcal/h</b>
1	0,85985
1,163	1

**Pressure, p.**

<b>Pa</b>	<b>kPa</b>	<b>bar</b>	<b>mWG</b>
1	0,001	0,00001	0,0001
1.000	1	0,01	0,1
100.000	100	1	10
10.000	10	0,1	1

**Flow, Q (φ).**

<b>l/s</b>	<b>m<sup>3</sup>/h</b>
1	3,6
0,278	1

**Temperature, t (θ).**

<b>Kelvin K</b>	<b>Celsius °C</b>
0	-273,15
273,15	± 0
373,15	100

**Greek alphabet.**

A α	B β	Γ γ	Δ δ	E ε	Z ζ	H η	Θ θ	I τ
alfa	beta	gamma	delta	epsilon	seta	eta	theta	iota
K κ	Λ λ	M μ	N ν	Ξ ξ	O ο	Π π	Ρ ρ	Σ σ
kappa	lamda	my	ny	xi	omikron	pi	ro	sigma
T τ	Υ υ	ϕ φ	X χ	Ψ ψ	Ω ω			
tau	ypsilon	phi	chi	psi	omega			

**Physical properties for water.**

Temperature t °C	Pressure p kPa	Density ρ kg/m <sup>3</sup>	Isobaric heat capacitivity c <sub>p</sub> J/ (kg x K)
0	-	999,84	4218
10	-	999,70	4192
20	-	998,205	4182
30	-	995,65	4178
40	-	992,2	4178
50	-	998,14	4181
60	-	983,21	4184
70	-	977,78	4190
80	-	971,80	4196
90	-	965,33	4205
100	1,3	958,35	4216
110	43,26	951,0	-
120	98,54	943,1	4245
130	170,11	934,8	-
140	261,36	926,1	4287
150	375,97	916,9	-



